

The iTPC Project: Mechanical Issues and a few solutions

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The TPC Today – inside the magnet with electronics & cables





The 'Naked' TPC





4.2 m long4.0 m diameter

The sectors were installed while the TPC was on the ground in B77

A (pretty good) clean room was built around the TPC for installation of the sectors

Critical Dimensions for the TPC



| Item | Dimension | Comment | |
|-------------------------------------|----------------------------------|--------------------------|--|
| Length of the TPC | 420 cm | Two halves, 210 cm long | |
| Outer Diameter of the drift volume | 400 cm | 200 cm radius | |
| Inner Diameter of the drift volume | 100 cm | 50 cm radius | |
| Distance: cathode to ground plane | 209.3 cm | Each side | |
| Cathode | 400 cm diameter | At the center of the TPC | |
| Cathode potential | 28 kV | typical | |
| Drift gas | P10: 90% Ar, 10% CH ₄ | He-Ethane as an option | |
| Drift Velocity | 5.45 cm/µsec | typical | |
| Transverse diffusion (σ) | 230 μm/√cm | 135 V/cm & 0.5 T | |
| Longitudinal diffusion (σ) | 360 μm/√cm | 135 V/cm & 0.5 T | |
| Magnetic Field | 0, ±0.25 T, ±0.5 T | Solenoidal | |

| Weight of TPC (lb) | | | | | |
|------------------------|----------|-----------------|-------------------------|-------------------------|----------------------|
| ltem | Max LBNL | Max BNL Lift | Installed Wt. w/ CTB | Installed Wt. w/ TOF | Basis |
| IFC | 107 | 107 | 107 | 107 | close est |
| OFC | 4991 | 4991 | 4991 | 4991 | close est |
| Wheel | 3100 | 3100 | 3100 | 3100 | measured |
| Wheel Brkts/Adj | 227 | 227 | 227 | 227 | rough est |
| TOF rails | 1080 | 1080 | 1080 | 1080 | exact |
| Outer Sectors | 2520 | 2520 | 2520 | 2520 | measured |
| Inner Sectors | 1752 | 1752 | 1752 | 1752 | close est 75# ea, |
| Gas Manifolds at wheel | 0 | 0 | 200 | 200 | removed for lift |
| FEE | 128 | 1539 | 1539 | 1539 | measured |
| FEE Manifolds | 480 | 480 | 480 | 480 | rough |
| RDO | 51 | 607 | 607 | 607 | close est. |
| RDO manifolds | 15 | 360 | 360 | 360 | rough |
| RDO/FEE Cable | 39 | 468 | 468 | 468 | close est |
| Dist Manif/hose | 240 | 390 | 390 | 390 | rough |
| CTB modules (120 ea.) | 0 | 6 60 | 3960 | 0 | measured/ 33# ea. |
| TOF modules (120 ea.) | 0 | 0 | 0 | 4800 | Est, G.Mutchler 9/98 |
| TOF cables/hose | 0 | 0 | 240 | 240 | rough |
| RDO elect. brkts | 24 | 24 | 24 | 24 | rough |
| SVT, Cone Assy &SSD | 0 | 0 | 365 | 365 | Mech Des Rev 3/98 |
| FTPC | 0 | 0 | 809 | 809 | FDR action item 1 |
| TOTAL | 14753 | 18304 | 22409 | 23249 | |

Goal: Hermetic coverage & better acceptance





- The outer pad plane is hermetic ... while the inner pad plane is not
 - Increase the segmentation on the inner pad plane
 - Renew the inner sector wires which are showing signs of aging

The upgrade will provide better momentum resolution, better dE/dx resolution, and improved acceptance at high η





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Inner sector detail





Inner sector construction: electrical & mechanical





Figure 40: Experts examining a spare inner sector for the TPC. Note the old style pad plane with electronics cards (ABDB boards) mounted along the edge of the sector. Normally the spare sectors (STAR has two spare sectors) are sealed in a storage box and kept under dry nitrogen.

Inner / Outer sector detail





- Note that inner and outer pad planes not at the same height
- Pad plane to anode plane (etc) distance not the same (4/4/6 vs 2/2/6)
- 3 mm gap between sectors, this is an issue during installation

Sector Wire Geometry – special notes





Wires are phase locked to the pad locations. 4 wires located over each pad row. We can probably tolerate a phase shift of 200 microns.

Ground wires lie directly over the Anode wires to limit sparking (Alice did it differently and had a problem)

Parameters for the old and new sectors



| Item | Inner | Outer | iTPC | Comment |
|---------------------------------|-------------|-------------|-------------|--------------|
| Pad Pitch (center to center) | 3.35 x 12 | 6.70 x 20 | 5.0 x 16 | mm |
| Isolation gap between pads | 0.5 | 0.5 | 0.5 | mm |
| Pad Size | 2.85 x 11.5 | 6.20 x 19.5 | 4.5 x 15.5 | mm |
| Number of Pads | 1750 | 3940 | 3496 | |
| Anode to pad plane spacing | 2 | 4 | 2 | mm |
| Anode voltage | 1170 V | 1390 V | ~ 1120 V | 20:1 S/N |
| Anode Gas Gain | 3770 | 1230 | ~ 2000 | nominal |
| Anode Wire diameter | 20 µm | 20 µm | 20 µm | Au plated W |
| Anode Wire pitch | 4 | 4 | 4 | mm |
| Anode Wires phase locked to pad | 3 wires, #2 | 5 wires, #3 | 4 wires, | grp centered |
| location | over center | over center | over center | over the pad |

Pad Plane & wire planes must be flat to better than 20 μ m to keep dE/dx resolution uniform to 1%

| Wire | Diam. (µm) | Pitch (mm) | Composition | Tension (N) |
|----------------------|---------------|---------------|-----------------|----------------|
| Anodes | 20 | 4 | Au-plated W | 0.50 |
| Anodes— last wire | 125 | 4 | Au-plated Be-Cu | 0.50 |
| Ground plane | 75 | 1 | Au-plated Be-Cu | 1.20 |
| Gating grid | 75 | 1 | Au-plated Be-Cu | 1.20 |

Grid Leak





Figure 29: A detailed view of the gap between the inner and outer sectors. Note that there is a 16 mm gap between the end of the gated grid in the inner sector and the start of the gated grid in the outer sector. Also, note that the last anode wire is larger in diameter (125 μ m) than the rest of the anode wires (20 μ m).

- Two improvements to the grid leak problem are possible
 - Add more large diameter wires (125 μ m) at top and bottom of grid
 - Install a wall between the inner and outer sector with bias rings
 - Simulations required and mechanical integration to be done

The Alice Solution to the Grid Leak problem



- Multiple thick anode wires near the boundaries of the sectors
- A wall to terminate the field lines from the Anode wires with ground potential and "cover" potential (match field gradient)



STAR MWPC Detail (outer sector shown)

1-0 1201V+2



Wire frame mounts pinned to the outside edge of the sector

VIDEBBOON SERVE

- 🗡 Anodes
 - No field shaping wires

Ground Plane of Wires

- Simple and reliable
- Individually terminated anode wires limit cross-talk
- Low gain

Gating Grid

- Inner Sector gain: 3000 at 1150 volts
- Outer Sector gain: 1100 at 1380 volts

Pad Plane



Grids stop here, last anode is larger diameter wire



| 2.0.000 | 0110201 | | | | 1 1 |
|----------------|---------|--------------------------------|---------------------|--------------|------------------|
| | | RHIC-STAR-TPC | | | |
| | | OUTER SECTOR | | | |
| 24A051- | SR0204 | GATED GRID WIRE MOUNT, LEFT | J. BOEHM | J. BERCOVITZ | |
| | | RHIC-STAR-TPC | | | |
| | | OUTER SECTOR | | | |
| 24A052- | SR0204 | GATED GRID WIRE MOUNT, RIGHT | J. BOEHM | J. BERCOVITZ | |
| | | RHIC-STAR-TPC | | | |
| | | OUTER SECTOR | | | |
| 24A053- | SR0204 | WIRE MOUNT INSULATING BOARD | J. BOEHM | J. BERCOVITZ | |
| | | OUTER AND INNER SECTOR WIRE | | | |
| 24A054C | SR0204 | MOUNT PIN, TAPERED | J.BOEHM J.BERCOVITZ | | April 2nd, 1993 |
| 24A055B | | RHIC-STAR-TPC | | | |
| 24A055A | | INNER AND OUTER SECTOR | | | |
| | SR0204 | WIRE GRID CONFIGURATION | J. BOEHM | J. BERCOVITZ | |
| | | RHIC-STAR-TPC | | | |
| | | TPC END WHEEL | | | |
| 24A056A | SR0204 | SECTOR SURVEY TARGETS LOCATION | J. BOEHM | J. BERCOVITZ | |
| | | RHIC-STAR-TPC | | | |
| | | OUTER SECTOR ASSEMBLY | | | |
| 24A057- | SR0204 | COOLING MANIFOLD MACHINING | J. BOEHM | J. BERCOVITZ | |
| | | RHIC-STAR-TPC | | | |
| | | COOLING MANIFOLD ASSEMBLY | | | |
| 24A058- | SR0204 | HEADER PORT, LEFT | J. BOEHM | J. BERCOVITZ | |
| | | RHIC-STAR-TPC | | | |
| | | COOLING MANIFOLD ASSEMBLY | | | |
| <u>24A059-</u> | SR0204 | HEADER PORT, RIGHT | J. BOEHM | J. BERCOVITZ | |
| | | RHIC-STAR-TPC | | | |
| | | OUTER SECTOR | | | |
| | | WINDER PLATFORM SUPPORT FRAME | | | |
| <u>24A060-</u> | SR0402 | (30.5 X 48) | R. CAYLOR | | March 24th, 1993 |
| | | RHIC-STAR-TPC | | | |
| | | OUTER SECTOR | | | |
| | | WINDER PLATFORM SUPPORT FRAME | | | |
| <u>24A061-</u> | SR0402 | (48 X 96) | R. CAYLOR | | |
| | | RHIC-STAR-TPC | | | |
| | | OUTER SECTOR | | | |
| <u>24A062-</u> | SR0402 | MOUNTING WHEEL END SUPPORT | R. CAYLOR | | |
| | | RHIC-STAR-TPC | | | |
| | | OUTER SECTOR | | | |
| <u>24A063-</u> | SR0402 | WIRE FRAME - 30 X 45 ID | R. CAYLOR | | March 11th, 1993 |
| | | | | | |

- We have a nearly complete collection of all mechanical drawings in pdf and dwg format (probably 90% of all components)
- We have copies of all of the electrical drawings (paper copies, due to obsolescence of electronic formats, circa 1993)

The Strongback ... yes, we can do it :-)





Figure 39: A prototype inner sector strongback is shown during fabrication at the University of Texas (circa 2013). The sector was machined out of a single piece of aluminum. Dimensions are: ~27 inches tall, ~25 inches wide and weight 73 lbs. The sector is viewed from the backside; the side upon which the electronics and cooling manifolds will eventually be mounted.

Prototype Strongbacks built at UTA





Prototype Strongbacks built at UTA in 2013





Can we adopt a radical new design?





- Eric Anderssen was asked to analyze the case with zero thickness Aluminum on the front face & no ribs
- The TPC is overpressurized to prevent leaks (2 mBar)
- This leaves only the G10 (0.125" thick) to support the excess pressure in the TPC



- Deflection due to pressure changes in the TPC leads to 300 μ m bulge
- Can be reduced by 8x with a rib ... but still not enough

No. A radical new design does not work ... and is not useful

Jim Thomas - LBL

Distortions due to wire tension ... do we need ribs?



With ribs, G10 & 0.1" Al

Without ribs, but with G10 and 0.1" AI

Figure 42: Simulated distortions in a proposed iTPC strongback due to the tension on the wire grids. The figure shows the result with the original rib design on the left, and without ribs on right. The maximum displacement of the pad plane, with ribs, is 4.6 microns. The deformation of the padplane without ribs is less, only 1.6 microns. Summary: ribs are not needed to support the tension on the wires. Simulations courtesy of Howard Wieman.

No, ribs are not needed to support the tension on the wires



2 mBar over-pressure (again) ... do we need ribs?





With ribs, G10 & 0.1" AI

Without ribs, but with G10 and 0.1" AI

Figure 43: Simulated distortions in a proposed iTPC strongback due to an excess pressure of 2 mBar inside the TPC. With ribs, we see a maximum distortion of 9.5 microns. Without ribs, the distortion grows to 16.5 microns. Simulations courtesy of Howard Wieman.

Yes, ribs are not needed to support the pressure inside the TPC but their height can be reduced ... and a radial rib may be better

Lumpy mass distribution ... ribs are important





Figure 41: Radiation length vs. eta for the original strongback. Electronics, cables and cooling manifolds are not included in these calculations. The lowest points are the cutouts for the electronics ... and so these numbers are not representative of the final assembly because this is where the FEE cards will sit and their **average** thickness is greater than 7%.

3/8" front face of AI is 10.5% Rad Length, G10 0.5% and small angle \Rightarrow 13%

Average mass distributions (±10°, 1.5 < η < 2.0)



| Total | 19.15% |
|----------------------|----------------|
| FEE sub Total | 7.65% |
| Cables | ~1% (estimate) |
| Sector Aluminum | 3.20 % |
| Sector G10 | 0.45 % |
| Ribs | 2.70 % |
| RDO card | 0.90 % |
| Cooling manifold | 3.25 % |
| FEE socket | 0.15 % |
| FEE rib | 0.45 % |
| FEE mounting bracket | 3.45 % |
| FEE | 3.60 % |

Table 6: The *average* radiation length budget for the components associated with a TPC inner sector (circa 1993) averaged over the fiducial volume of the sector. The average takes out the lumps in the mass distribution (for better or worse) but also illustrates how the budget for the Al on the front face compares to the electronics and cooling budget. The sector data have been averaged over a range from $1.5 < \eta < 2.0$ and $-10 < \phi < 10$ degrees. Geant simulations courtesy of Irakli Chakaberia.

Three candidates for reduction: FEE mounting bracket, Sector Aluminum and Ribs. It does not make sense to reduce sector AI to less than 3/16" (5% absolute, 1.6% average)

Decisions, decisions ...



- Decisions need to be made before the strongback design is final
 - Thickness of front face (recommend 3/8" (5mm))
 - Height of ribs & location ... analysis needed but perhaps 1 cm high will work
 - Final decision needed on location of holes for electronics because it affects the location of the ribs, spider mounts and optical targets
 - Choose new location for spider mounts and optical target
 - Check that the sector can be installed without damage
 - satisfies clearance checks, is stable, and is strong enough
 - For example, sector insertion should not interfere with TPC endwheel
- Timeline
 - UT can fabricate 1 sector per month. We need 24 + spares.
 - Fabrication should start soon
- Optimistic note: we can proceed with the strongback fabrication in 2 steps, i.e. touch the strongback multiple times. 1.) Hog out AI in the middle, 2.) apply finishing touches.
 - Need to carefully to think out step 1 so that it doesn't interfere with step 2 (example: thickness of ribs, spider mounts and location of electronics). Also don't want to build something that cannot be installed. Have to understand spider mounts and insertion tool before finalizing design and approving fab.



- The assembly of the TPC sectors relied upon an outstanding group of senior technicians with good hands and a wealth of experience.
- Like most wire chamber techniques, many of these techniques have not been academically documented
 - Example: what kind of epoxy to use, how to prepare large amounts of the epoxy and store it, how to apply it
 - Combs for aligning the wires over the pad plane
 - Holding pad plane flat to 10 microns
 - Alignment of pad planes with strongback while gluing (50 microns)
- We have to learn, document and share these techniques
 - Unique, one of a kind fabrications
 - Physicists are not good at this stuff
 - Outstanding technicians are required

Granite table ... the secret ingredient





The pad plane must be held flat on the table with vacuum

- One of the original granite tables is stored in the basement at BNL
- Black granite is preferred
 - contains less water and thus parts don't rust so quickly
- Dimensions (at BNL)
 - 60 x 42 x 8 inches
 - 36 inches off the floor (floor to top surface) although this is probably not critical
- Grade A surface plate, see:
 - <u>http://www.precisiongraniteusa.com/Products.aspx</u>
 Grade A "Inspection Grade" is defined here
 - <u>http://precisiongraniteusa.com/pdffiles/fed_spec.pdf</u>
- Flat to 10 μm (!)
- Original manufactured by Mojave Granite
 - 1651 Miller Ave, Los Angeles CA
- Fortunately, several manufacturers of granite tables in Shandong province.

Granite table, tooling balls and platform guards





Comb and Tooling Balls exposed - note: table has 2 combs



Teeth on the comb





Comb plate and top of straight edge plate shown at left. "Bottom" of comb is below the level of the straight edge.

Teeth on the comb have an asymmetrical shape – one edge is vertical but the other is well-rounded.

Wires will rest on the top surface of the straight edge

Wires are laid on the straight edge then "slid" to contact the vertical sides of comb

Loose wires are pushed into contact with the comb using a brush



Pitch between teeth exactly 1 mm Depth of teeth about 1 mm Note that the height of the straight edge is about half way up the tooth



Platform Guards

 The guards protect the wire planes, provide a hand-rest for gluing the wire planes and for soldering the gated grid

Comments

- Plates are ¼ inch thick: the plates bend by about 2 to 3 mm when a person leans on them
- 2 inch diameter cylinders + washers were used to adjust the elevation of the platform guards.
- There will probably be 3 different granite tables in use to build the iTPC sectors (one for each grid height). Each table may have different size spacers for the platform guards





- Fixing the grid leak on the inner sector will change the mechanical design of the strongback
 - Not a problem ... we just have to remember to do it and check that it is compatible with the clearance between sectors
- Hopefully, the fix for the grid leak does not affect the installation procedure ... but we will have to check it carefully because the "wall" does change the shape of the sector
 - Installation is tricky and requires the sector to move in many odd directions before it is finally bolted into place.
- The Ground Wires are at the same elevation on the inner and outer sectors, ditto Gated Grid wires ... have to keep it this way
- Tolerances for the flatness of the padplane and the height of the wires above the padplane are very demanding

Sector Insertion – special tools required





The STAR Magnet – life was simple and clean



- The old insertion tool was designed for use on the floor and required a crane to support the tool
- It is not practical to remove the TPC from the magnet for the iTPC upgrade
- The STAR TPC sits inside the magnet with an offset of 52 inches from the face of the magnet
- A new approach is needed
- See talk by Rahul





- We can do this
- We have the drawings
- We have learned many of the secret ingredients
 - No doubt, a few of the most clever design features are still to be discovered
 - No doubt, a few of the most difficult fabrication techniques still need to be discovered
- We have made a good start on the design of the new sector
 - Final design requires analysis and input from professionals
- We need good hands
 - Unique, one of a kind, fabrications and assembly techniques
- We need time
- And we need money